

Harbor View Estates

PUMP STATION And SPECIFICATIONS

ALSE JOB # 30147E



HARBOR VIEW ESTATES

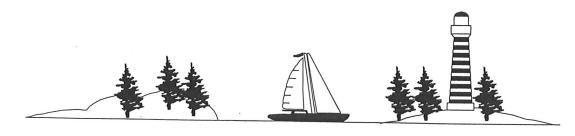
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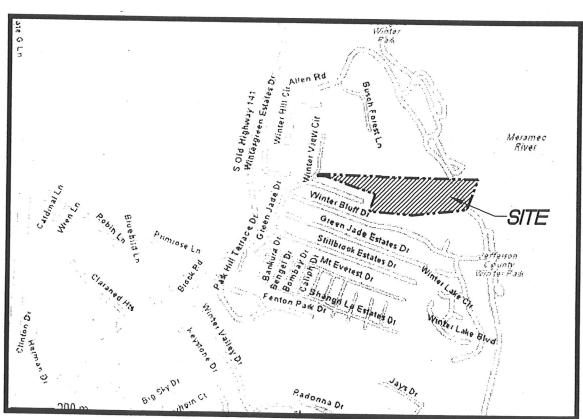
Date: September 26, 2007 Revised Date: December 27, 2007

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HARBOR VIEW ESTATES



LOCATION MAP

1.1 SEWER SYSTEM INFORMATION

B. INTRODUCTION:

1 Introduction

The proposed Harbor View Estates Subdivision is a residential development consisting of 48 single family lots. The waste water of this subdivision is flowing to a lift station located within the development via a 3,147 lineal feet of 8 inch PVC gravity sewer. The pump station will convey sewage via a 3.0" PVC, schedule 40 force main to an existing manhole located in common ground near backyard of the proposed lot#40 of this development. This report will provide the engineering design and specifications necessary to construct this pump station and force main line.

2 Existing Sewer System

Existing manhole located in common ground near proposed lot#40 of this development.

3 Future Sanitary Sewer Services

There is no additional flow to this lift station.

E. DESIGN SUMMARY:

1 Average Daily Flow:

a) Average Daily Flow:

Pe = Nb x Np = 48 residential units x 3.7 persons per unit
Pe = 177.6 persons

$$F = 177.6$$
 persons x 100 gallons/person/day = 17,760 gpd
 $I = 8in. X (3,147/5,280)mi. x 200 = 954 gpd$
Total = 18,714 gpd
Or 13.00 gpm

2 Total Peak Daily Flow:

$$PDF = 4.0 \times ADF = 4.0 \times 18,714 \text{ gpd} = 74,856 \text{ gpd}$$

Or 51.98 gpm

3 Volume for 24 Hour Detention:

Not required for this project because a 50 KW natural gas electric generator will be installed as a second source of supplying power for this lift station.

4 Static Head:

The maximum elevation of the force main line =
$$494.00$$

The pump of shut off elevation = 410.45
Static Head = $494.00 - 410.45 = 83.55$ (worst case)

5 Total Dynamic Head:

See Tables 5.1 and 5.2: Dynamic Head for best case and worst case conditions.

6 Selected Pump Manufacture's Information:

The pump selected is a Myers

Model WG50H-21-25, 5 HP, 6.00" Dia. Impeller

Submersible Grinder pump

Horsepower = 5.0 hp

3450 rpm

230 volt, 1 phase

Optimum Discharge Rate

Worst case: 62 gpm @ 113 ft of head (1 pump)

77 gpm @ 126 ft of head (2 pumps)

Best case: 69 gpm @ 108 ft of head (1 pump)

92 gpm @ 121 ft of head (2 pumps)

7 Pump Cycle Times

Volume of wetwell (pump on – pump off)
$$Vr = (25*3.14/4) (410.75-408.75)*7.481(gal/cf) = 293.63 gal.$$

Flow Cycle Time of Worst Case of Average Daily Flow:

Tf(min) = Vr/ADF = 293.63/13.0 = 22.59 min.

Tp (min) = Vr/(CSR-ADF) = 293.63/(62.0-13.0) = 5.99 min.

Cycle Time = 2 (Tf+Tp) = 2 (22.59+5.99) = 57.16 min.

Flow Cycle Time of Worst Case of Peak Daily Flow:

Tf (min) = Vr/ADF = 293.63/51.98 = 5.65 min.

Tp (min) = Vr/(CSR-ADF) = 293.63/(62.0-51.98) = 29.30 min.

Cycle Time = 2 (Tf+Tp) = 2 (5.65+29.30) = 69.90 min.

8 Force Main Information

See Attached plan Sheets for plan and profile diagrammatic.

9 Buoyancy Calculations

See appendix for buoyancy calculations.

DESIGN SUMMARY

- 1 Total Average Daily Flow = 18,714 gpd
- 2 Total Peak Daily Flow = 51.98 gpm
- 3 Static Head Hsb 81.6' Hsw = 83.6'
- 4 Total Dynamic Head: TDHb = 108' TDHw= 113'
- 5 The pump selected is a Myers

Model WG50H-21-25, 5 HP, 6.00" Dia. Impeller Submersible Grinder pump Horsepower = 5.0 hp 3450 rpm 230volt, 1 phase Optimum Discharge Rate Worst case: 62 gpm @ 113 ft of head (1 pump)

Worst case: 62 gpm @ 113 ft of head (1 pump) Best case: 69 gpm @ 108 ft of head (1 pump)

6 Pump Cycle Times:

Average Daily Flow Cycle Time = 2 (Tf+Tp) = 2 (22.59+5.99) = 57.16 min.Peak Daily Flow Cycle Time = 2 (Tf+Tp) = 2 (5.65+29.30) = 69.90 min.

7 Force Main Information:

See Attached plan sheets for Plan and Profile Diagram

8 Buoyancy Calculations:

See Appendix for buoyancy calculations.

PDF (gal/min)	Harbor View	UMP CYCLE TIMES Estates p Station Design Data.	
ADF (gal/day) or (gal/min) 13.00 PDF (gal/min) 51.98 (gal/min)	Flows		
or (gal/min) PDF (gal/min) case) Finished Floor Elevation Top Elevation Flowline Elevation In High Water Alarm Lag Pump On Lead Pump On Lead and Lag Pump Off Volumes Dia. of Pump Station (ft) (Equivalent Storage per foot (gal) Normal Operating Volume (gal) (Lead Pump On Stop) Total Storage (Invert - Stop)(gal) Total Storage time at ADF (min.) Total Storage time at PDF (min.) Total Time - Alarm to overflow at PDF Flow (gpm) Pump on (min), Tp Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp Pump off (min), Tp	1 10W5	ADF (gal/day)	18714
PDF (gal/min) case)			13.00
Finished Floor Elevation			51.98
Finished Floor Elevation Top Elevation Top Elevation Top Elevation Flowline Elevation In Flowline Elevation Out 421.76 High Water Alarm Lag Pump On Lead Pump On Lead and Lag Pump Off 410.45 Volumes Dia. of Pump Station (ft) (Equivalent Storage per foot (gal) Normal Operating Volume (gal) (Lead Pump On - Stop) Total Storage (Invert - Stop)(gal) Total Storage time at ADF (min.) Total Storage time at PDF (min.) Total Time - Alarm to overflow at PDF Storage Times Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tp		case)	62
Finished Floor Elevation Top Elevation Top Elevation Top Elevation Flowline Elevation In Flowline Elevation Out 421.76 High Water Alarm Lag Pump On Lead Pump On Lead and Lag Pump Off 410.45 Volumes Dia. of Pump Station (ft) (Equivalent Storage per foot (gal) Normal Operating Volume (gal) (Lead Pump On - Stop) Total Storage (Invert - Stop)(gal) Total Storage time at ADF (min.) Total Storage time at PDF (min.) Total Time - Alarm to overflow at PDF Storage Times Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tp	Flevations		
Top Elevation	Licvations	Finished Floor Elevation	424.50
Flowline Elevation In			425.20
High Water Alarm			416.20
Lag Pump On 412.95 Lead Pump On 410.45 Volumes Dia. of Pump Station (ft) (Equivalent 5.0000 Storage per foot (gal) 146.81 Normal Operating Volume (gal) (Lead Pump On - Stop) 293.63 Total Storage (Invert - Stop)(gal) 844.18 Total Storage time at ADF (min.) 22.55 Total Storage time at PDF (min.) 5.65 Total Time - Alarm to overflow at PDF 33.15 Cycle Times Flow (gpm) 13.00 Pump on (min), Tp 5.95 Pump off (min), Tf 22.55 Cycle time (min) = 2*(Tp + Tf) 57.16 Flow (gpm) Pump on (min), Tp 9.18 Pump off (min), Tf 7.34 Cycle time (min) = 2*(Tp + Tf) 13.35 Pump on (min), Tp 29.30 P		Flowline Elevation Out	421.78
Lag Pump On 412.95 Lead Pump On 410.45 Volumes Dia. of Pump Station (ft) (Equivalent 5.0000 Storage per foot (gal) 146.81 Normal Operating Volume (gal) (Lead Pump On - Stop) 293.63 Total Storage (Invert - Stop)(gal) 844.18 Total Storage time at ADF (min.) 22.55 Total Storage time at PDF (min.) 5.65 Total Time - Alarm to overflow at PDF 33.15 Cycle Times Flow (gpm) 13.00 Pump on (min), Tp 5.95 Pump off (min), Tf 22.55 Cycle time (min) = 2*(Tp + Tf) 57.16 Flow (gpm) Pump on (min), Tp 9.18 Pump off (min), Tf 7.34 Cycle time (min) = 2*(Tp + Tf) 13.35 Pump on (min), Tp 29.30 P		High Water Alarm	413.45
Lead Pump On			412.95
Lead and Lag Pump Off			412.45
Dia. of Pump Station (ft) (Equivalent 5.0000 Storage per foot (gal) 146.81 Normal Operating Volume (gal) (Lead Pump On - Stop) 293.63 Total Storage (Invert - Stop)(gal) 844.18 Total Storage time at ADF (min.) 22.58 Total Storage time at PDF (min.) 5.66 Total Time - Alarm to overflow at PDF 33.19 Cycle Times Flow (gpm) Pump on (min), Tp Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp Pump off (min), Tp Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp Pump off (min), Tp Pump off (min), Tf Solution Solution Total Storage (Invert - Stop) (gal) Red. 18 R		•	410.45
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Normal Operating Volume (gal)			
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Total Storage time at ADF (min.) Total Storage time at PDF (min.) Total Time - Alarm to overflow at PDF Flow (gpm) Pump on (min), Tp Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp Pump off (min), Tp Pump off (min), Tp Pump off (min), Tf Solution		,	
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Pump on (min), Tp Pump off (min), Tf 22.59 Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp Pump off (min), Tf Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp Pump on (min), Tp Pump off (min), Tf Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump off (min), Tf T.34 Cycle time (min) = 2*(Tp + Tf) Flow (gpm) Pump on (min), Tp 29.30 Pump off (min), Tf Flow (gpm) Pump off (min), Tf	Cycle Times		
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Pump on (min), Tp 9.18 Pump off (min), Tf 9.79 Cycle time (min) = 2*(Tp + Tf) 37.93 Flow (gpm) 40.00 Pump on (min), Tp 13.35 Pump off (min), Tf 7.34 Cycle time (min) = 2*(Tp + Tf) 41.38 Flow (gpm) 51.98 Pump on (min), Tp 29.30 Pump off (min), Tf 5.65		Flow (apm)	30.00
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Pump on (min), Tp 13.35 Pump off (min), Tf 7.34 Cycle time (min) = 2*(Tp + Tf) 41.35 Flow (gpm) 51.95 Pump on (min), Tp 29.30 Pump off (min), Tf 5.65		Flow (apm)	40 00
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Pump on (min), Tp 29.30 Pump off (min), Tf 5.65			41.38
Pump on (min), Tp 29.30 Pump off (min), Tf 5.65		Flow (apm)	51 98
Pump off (min), Tf 5.65			
1 (//			5.65
Cycle time (min) = $2*(Tp + Tf)$ 69.91			69.91

1/3/2008

Harbor View Estates

Residential Lift Station Design Data, Bouyancy Calculations

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1 Ww = Weight of concrete wet well
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- 2 Wf = Weight of concrete Bottom slab
- 3 We = Weight of earth backfill on footing
- 4 Wt = Ww + We + Wf (or weight of detention chambers and backfill overburden)
- 5 Ws = Weight of displaced water
- 6 Wt = Should be greater than Ws
- 1 Weight of Concrete Wet Well

Top Elevation =	425.20
Bottom Elevation =	408.95
Total Height	16.25 Ft.

Wt /Ft. of 5' Dia. Wet Wel 1,780.50 Lbs./Ft.

Wt. of 1 CY of Conc. 4,050.00 Lbs.

Wt. of Wet Well 32,983.13 Lbs.

2 Weight of Bottom Slab

Area of Base 31.47 Ft².

Thickness of Base 8 In.

Wt. Of Conc. 150 Lbs./CF

Wt. Of Base 3,147 Lbs.

3 Weight of Earth on Base

Weight of Earth 0 Lbs.

4 Weight Total

Wt = Ww + We + Wf (or weight of detention chambers and backfill overburden)

Wt = 36,130 Lbs.

5 Force Bouyant

Volume Displaced 559.37 Cu. Ft. Weight of Water 62.4 Lbs./Cu. Ft.

Bouyant Force 34905

6 Check Bouyancy

Wt Fb 36,130.13 > 34,904.53 OK

7 Total Bearing

Total Wt. of Station Total Area of Base Lbs/Sq. Ft.

71,035 Lbs. 31.47 Sq. Ft. 2257.218 <3000 OK

12/31/2007

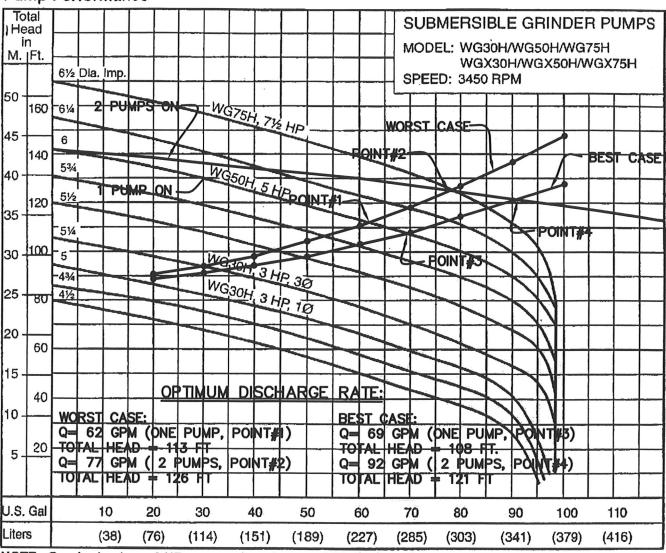
APPENDIX - D3 HARBOR VIEW ESTATES SYSTEM HEAD CALCULATIONS AND CURVES

Lift Statio	n Informat	Recipient Manhole Information				Head Loss Due to Station Piping (5ft/sec) 3.77					
Top Elev. Flowline in Flowline ou Alarm on E Lag pump 0 Lead pump Pump off E	Elev. ut Elev. lev. On El.	425.20 416.20 421.78 413.45 412.95 412.45 410.45	Flowline out I	Flowline in Elev. 475.31 Flowline out Elev. 475.31 max elev 494.00 H-W Coeff. (Worst Case) 120				es (per 100') = s = H _L = C _L (V ² /2	0.2083(100/C) 2g)	^{1.85} xQ ^{1.85} /D ^{4.86}	155
Flow input From Subdivision ADF= PDF= Pipe Dia.	18,714 52.0	gpd (or) = gpm in.	13.0	gpm							
Q	d	С	L	V	Minor	F		Static		Static	
flow rate	pipe	H-W	Len.	Velocity	Head	Friction	Total	Head	System	Head	System
gpm	diameter	Coeff.	Pipe	In Pipe	Losses	Head	System	Elev	Head	Elev	Head
	inches				this length	this length	Head	Pump On	Pump on	Pump off	Pump off
0	3.068	120	1862	0.00	0.000	0.00	3.77	81.6	85.3	83.6	87.3
20	3.068	120	1862	0.87	0.077	3.02	6.86	81.6	88.4	83.6	90.4
25	3.068	120	1862	1.08	0.121	4.57	8.45	81.6	90.0	83.6	92.0
30	3.068	120	1862	1.30	0.174	6.40	10.34	81.6	91.9	83.6	93.9
35	3.068	120	1862	1.52	0.236	8.51	12.51	81.6	94.1	83.6	96.1
40	3.068	120	1862	1.74	0.309	10.89	14.97	81.6	96.5	83.6	98.5
45	3.068	120	1862	1.95	0.391	13.55	17.70	81.6	99.3	83.6	101.3
50	3.068	120	1862	2.17	0.483	16.46	20.71	81.6	102.3	83.6	104.3
55	3.068	120	1862	2.39	0.584	19.64	23.99	81.6	105.5	83.6	107.5
60	3.068	120	1862	2.60	0.695	23.07	27.53	81.6	109.1	83.6	111.1
65	3.068	120	1862	2.82	0.816	26.75	31.33	81.6	112.9	83.6	114.9
70	3.068	120	1862	3.04	0.946	30.68	35.39	81.6	116.9	83.6	118.9
75	3.068	120	1862	3.25	1.086	34.85	39.71	81.6	121.3	83.6	123.3
80	3.068	120	1862	3.47	1.235	39.27	44.27	81.6	125.8	83.6	127.8
85	3.068	120	1862	3.69	1.395	43.94	49.10	81.6	130.6	83.6	132.6
90	3.068	120	1862	3.91	1.564	48.84	54.16	81.6	135.7	83.6	137.7
95	3.068	120	1862	4.12	1.742	53.97	59.48	81.6	141.0	83.6	143.0
100	3.068	120	1862	4.34	1.930	59.35	65.04	81.6	146.6	83.6	148.6
	3.068	120	1862	4.56	2.128	64.95	70.85	81.6	152.4	83.6	154.4
105											
105 110	3.068	120	1862	4.77	2.336	70.79	76.89	81.6	158.4	83.6	160.4

APPENDIX - D3 HARBOR VIEW ESTATES SYSTEM HEAD CALCULATIONS AND CURVES

Lift Station	Information		Recipient Manhole Information Head Loss Due to Station Piping (5ft/sec 3.77								
Top Elev. Flowline in I Flowline out	Elev.	425.20 416.20 421.78		Flowline in Elev. Flowline out Elev.			Friction losses (per 100') = 0.2083(100/C) ^{1.85} xQ ^{1.85} /D ^{4.8655} Minor losses = $H_L = C_L(V^2/2g)$				
Alarm on El	ev.	413.45	max elev			494.00					
Lag pump (On El.	412.95									
Lead pump	On El.	412.45	H-W Coe	ff. (Best Ca	ase)	150.00					
Pump off El	ev.	410.45									
Flow input in	nto system										
From											
Subdivision	10 711										
ADF=	18,714	0.									
PDF= Pipe Dia.	52.0 (3.068 i										
Ріре Біа.	3.000	ш.									
Q	d	С	L	V	Minor	F		Static		Static	•
flow rate	pipe	H-W	Len.	Velocity	Head	Friction	Total	Head	System	Head	System
gpm	diameter	Coeff.	Pipe	In Pipe	Losses	Head	System	Elev	Head	Elev	Head
-	inches				this length	this length	Head	Pump On	Pump on	Pump off	Pump off
0	3.068	150	1862	0.00	0.000	0.00	3.77	81.6	85.3	83.6	87.3
20	3.068	150	1862	0.87	0.077	2.00	5.84	81.6	87.4	83.6	89.4
25	3.068	150	1862	1.08	0.121	3.02	6.91	81.6	88.5	83.6	90.5
30	3.068	150	1862	1.30	0.174	4.23	8.17	81.6	89.7	83.6	91.7
35	3.068	150	1862	1.52	0.236	5.63	9.63	81.6	91.2	83.6	93.2
40	3.068	150	1862	1.74	0.309	7.21	11.28	81.6	92.8	83.6	94.8
45	3.068	150	1862	1.95	0.391	8.96	13.12	81.6	94.7	83.6	96.7
50	3.068	150	1862	2.17	0.483	10.89	15.14	81.6	96.7	83.6	98.7
55	3.068	150	1862	2.39	0.584	13.00	17.34	81.6	98.9	83.6	100.9
60	3.068	150	1862	2.60	0.695	15.26	19.73	81.6	101.3	83.6	103.3
65	3.068	150	1862	2.82	0.816	17.70	22.28	81.6	103.8	83.6	105.8
70	3.068	150	1862	3.04	0.946	20.30	25.01	81.6	106.6	83.6	108.6
75	3.068	150	1862	3.25	1.086	23.07	27.92	81.6	109.5	83.6	111.5
80	3.068	150	1862	3.47	1.235	25.99	30.99	81.6	112.5	83.6	114.5
85	3.068	150	1862	3.69	1.395	29.08	34.24	81.6	115.8	83.6	117.8
90	3.068	150	1862	3.91	1.564	32.32	37.65	81.6	119.2	83.6	121.2
95	3.068	150	1862	4.12	1.742	35.72	41.23	81.6	122.8	83.6	124.8
100	3.068	150	1862	4.34	1.930	39.27	44.97	81.6	126.5	83.6	128.5
105	3.068	150	1862	4.56	2.128	42.98	48.88	81.6	130.4	83.6	132.4
110	3.068	150	1862	4.77	2.336	46.85	52.95	81.6	134.5	83.6	136.5 ,
115	3.068	150	1862	4.99	2.553	50.86	57.18	81.6	138.7	83.6	140.7

Pump Performance



NOTE: On single phase 3 HP pumps, do not exceed 5" dia, impeller.

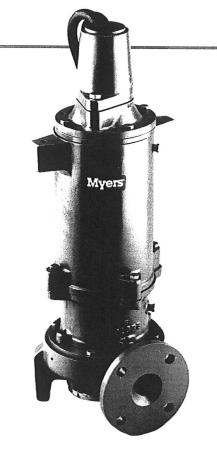
Available Models			Motor Electrical Data									
Standard	Explosion Proof	HP	Volts	Phase	Hertz	Start Amps	Run Amps	Run KW	Start KVA	Run KVA	NEC Code Letter	Service Factor
WG30H-21-25	WGX30H-21-25	3	230	1	60	82	21.0	4.3	41.9	4.8	G	1.4
WG30H-03-25	WGX30H-03-25	3	200	3	60	69	15.0	4.3	23.9	5.2	J	1.4
WG30H-23-25	WGX30H-23-25	3	230	3	60	53	13.0	4.3	21.1	5.2	Н	1.4
WG30H-43-25	WGX30H-43-25	3	460	3	60	26	6.5	4.3	20.7	5.2	Н	1.4
WG30H-53-25	WGX30H-53-25	3	575	3	60	21	5.2	4.3	21.0	5.2	Н	1,4
WG50H-21-25	WGX50H-21-25	5	230	1	60	122	32	6.3	28.1	7.4	G	1.7
WG50H-03-25	WGX50H-03-25	5	200	3	60	90	21.6	6.3	31.1	7.5	G	1.7
WG50H-23-25	WGX50H-23-25	5	230	3	60	78	18.8	6.3	27.0	7.5	G	1.7
WG50H-43-25	WGX50H-43-25	5	460	3	60	39	9.4	6.3	31.0	7.5	Ģ	1.7
WG50H-53-25	WGX50H-53-25	5	575	3	60	31	7.5	6.3	31.0	7.5	Ģ	1.7
WG75H-03-25	WGX75H-03-25	7.5	200	3	60	90	25.8	7.9	31.1	8.9	D	1.15
WG75H-23-25	WGX75H-23-25	7.5	230	3	60	78	22.4	7.9	27.0	8.9	D	1.15
WG75H-43-25	WGX75H-43-25	7.5	460	3	60	39	11.2	7.9	31.0	8.9	D	1.15
WG75H-53-25	WGX75H-53-25	7.5	575	3	60	31	9.0	7.9	31.0	8.9	D	1.15



F. MANUFACTURES SPECIFICATIONS AND CUT-SHEETS.

WG30H-75H and WGX30H-75H

Standard (WG30H-75H) and Explosion-proof (WGX30H-75H) 3-7½ HP, High-Head Submersible Grinder Pumps







(WGX30H-75H only)



YERS WG30H-75H ARE RUGGED 3-71/2 HORSEPOWER SUBMERSIBLE CENTRIFUGAL GRINDER PUMPS DESIGNED FOR RESIDENTIAL, COMMERCIAL OR INDUSTRIAL APPLICATIONS. They are especially suited for use in pressure sewer applications or in systems with long discharge runs or high static heads. The WG30H-75H feature a heavyduty cutter mechanism and recessed impeller design to efficiently grind typical sewage solids into a fine slurry.

The WG30H-75H grinder pumps are available in standard and U.L. Listed explosion-proof (WGX30H-75H), construction for use in Class 1, Group D hazardous locations.

WG30H-75H grinder pumps can be installed in a variety of packaged systems. Factory-assembled simplex or duplex packages with guide rail systems are available. Individual rail components are also available for installation in onsite concrete systems. F.E. Myers offers a complete line of submersible sump, sewage, effluent, grinder, non-clog wastewater pumps, controls, basins and accessories. For additional information, please contact your local Myers representative or the Myers Ashland, Ohio sales office at 419/289-1144.

ADVANTAGES BY DESIGN

IDEAL FOR USE IN PRESSURE SEWER SYSTEMS.

Recessed impeller provides steep non-overloading operating curve.

DURABLE MOTOR WILL DELIVER MANY YEARS OF RELIABLE SERVICE.

- Oil-filled motor for maximum heat dissipation and constant bearing lubrication.
- Recessed impeller reduces radial bearing loads; increases bearing life.
- High-torque capacitor start single phase or three phase motors for assured starting under heavy load.
- Seal leak probes and on-winding heat sensors warn of seal leak condition, and stop motor if motor over heats. Helps prevent costly motor damage.

THE WG30H-75H ARE DESIGNED FOR EASY MAINTENANCE.

Shredding ring and grinder impeller are replaceable without dismantling pump or motor.

PRODUCT CAPABILITIES

Capacities To	98 GPM	367 LPM		
Heads To	170 ft.	52.0 m		
Liquids Handling	domestic re	aw sewage		
Intermittent Liquid Temp.	up to 140°F	up to 60°C		
Winding Insulation Temp. (Class F)	311°F	155°C		
Motor Electrical Data (Single phase motors are capacitor start type. Myers control panels or panels or capacitor kits are required for proper operation and warranty.)	3450 RPM, 60 Hz 3-5 HP: 230V, 1 Ph 3-7 ¹ / ₂ HP: 208, 230, 460V, 3 Ph			
Std. Third Party Approvals Optional Approvals	UL Class 1 (WGX30H-75H o	, Group D		
Acceptable pH Range	6-	.9		
Specific Gravity	.9-1.1			
Viscosity	28-35 SSU			
Discharge (Flange Dim.)	2-1/2 in.	63.5 mm		
Min. Sump Dia. (Simplex) (Duplex)	36 in. 48 in.	91.4 cm 121.9 cm		

NOTE: Consult factory for applications outside of these recommendations.

Construction Materials	
Motor Housing, Seal Housing Cord Cap and Volute Case	cast iron, Class 30 ASTM A48
Impeller	recessed, bronze
Power Cord	25 ft. SOW/SOW-A
Control Cord	25 ft. SOW/SOWA
Mechanical Seals Standard Optional	double tandem, carbon and ceramic lower tungsten carbide
Pump, Motor Shaft	416 SST
Fasteners	300 Series SST
Shredding Ring and Grinder Impeller	440 SST, 58-60 Rockwell

WHERE INNOVATION MEETS TRADITION



WG30H-75H and WGX30H-75H

Standard (WG30H-75H) and Explosion-proof (WGX30H-75H) 3-7½ HP, High-Head Submersible Grinder Pumps

STATOR

3450 RPM, 1 and 3 phase. Press fit for perfect alignment and best heat transfer. Oil-filled motor conducts heat and lubricates bearings.

CABLE ENTRY SYSTEM

Provides double seal protection. Cable jacket sealed by compression grommet. Individual wires sealed by epoxy potting.

HEAT SENSOR

Protects motor from burnout due to excessive heat from any overload condition. Automatically resets when motor has cooled.

BALL BEARINGS

Upper and lower ball bearings support shaft and rotor and take axial and radial loads.

HEAVY 416 SST SHAFT

Corrosion resistant.
Reduces shaft deflection due to grinding loads.

SHAFT SEALS

Double tandem mechanical shaft seals protect motor. Oil-filled seal chamber provides continuous lubrication.

SEAL LEAK PROBES

Detect water in seal housing. Activates warning light in control panel. (Test resistor on UL Listed models.)

VOLUTE CASE

Cast iron; horizontal discharge. (Drilled for 21/2" pipe flange.

17

Grinder impeller and shredding ring are replaceable without dismantling pump. Constructed of 440 SST hardened to 56-60 Rockwell.

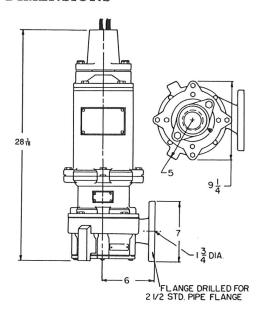
GRINDER ASSEMBLY SLEEVE BEARING

Takes radial load; provides flame path. (UL listed pumps only.)

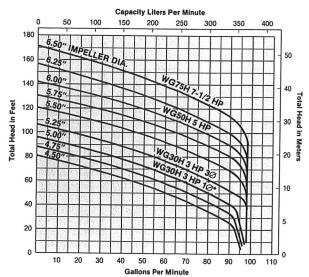
IMPELLER

Bronze recessed impeller handles ground slurry without clogging or binding. Provides unobstructed flow passage. Reduces radial loads. Pumpout vanes help keep trash from seal; reduces pressure at seal faces.

DIMENSIONS



PERFORMANCE CURVE



NOTE: On single phase 3 HP pumps do not exceed 5" diameter impeller.

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Myers ES-224 1 3/4 DIA. $9\frac{1}{4}$ FLANGE DRILLED FOR 2 1/2" STD. PIPE FLANGE $28\frac{1}{16}$ 7 DIA. $4\frac{15}{16}$ MIN. Myers Environmental Systems 6 MAX. LEGS OPTIONAL WG30H, WG50H, WG75H, WGX30H, WGX50H, WGX75H GRINDER PUMPS ES-224

WG30-75H GRINDER PUMP SPECIFICATIONS

120 501
PUMP MODEL - Pump shall be of the centrifugal type Myers model or equal with an integrally built in grinder unit and submersible type motor. The grinder unit shall be capable of macerating all material in normal domestic and commercial sewage including reasonable amounts of foreign objects such as small wood, sticks, plastic, thin rubber, sanitary napkins, disposable diapers and the like to a fine slurry that will pass freely through the pump and 2" discharge pipe. Discharge shall be standard 2½" flange.
OPERATING CONDITIONS - Pump shall have a capacity of GPM at a total head of shall use a 5 HP motor operating at 3450 RPM.
MOTOR - Pump motor shall be of the totally enclosed, submersible, squirrel cage induction type rated 5 horsepower at 3450 RPM, 60 Hz.
Motor shall be for single phase 230 volts or three phase 200 volts, 230 volts, 460 volts or 575 volts. Single phase motors shall be of capacitor start, capacitor run, NEMA L type. Three phase motors shall be NEMA B type.
Stator winding shall be of the open type with Class F insulation good for 155°C (311°F) maximum operating temperature. Winding housing shall be filled with a clean high dielectric oil that lubricates bearings and seals and transfers heat from windings and rotor to outer shell. Air-filled motors which do not have the superior heat dissipating capabilities of oil-filled motors shall not be considered equal.
Motor shall have two heavy duty ball bearings to support pump shaft and take radial and thrust loads and a sleeve guide bushing directly above the lower seal to take radial load and act as flame path for seal chamber. Ball bearings shall be designed for 50,000 hours B-10 life. Stator shall be heat shrunk into motor housing.
A heat sensor thermostat shall be attached to top end of motor winding and shall be connected in series with the magnetic contactor coil in control box to stop motor if motor winding temperature reaches 221°F. Thermostat to reset automatically when motor cools. Three heat sensors shall be used on 3 phase motors.
The common motor pump and grinder shaft shall be of #416 stainless steel threaded to take pump impeller and grinder impeller.
<u>SEALS</u> - Motor shall be protected by two mechanical seals mounted in tandem with a seal chamber between the seals. Seal chamber shall be oil filled to lubricate seal face and to transmit heat from shaft to outer shell.
Seal face shall be carbon and ceramic and lapped to a flatness of one light band. Lower seal faces shall be carbide (optional).
A double electrode shall be mounted in the seal chamber to detect any water entering the chamber through the lower seal. Water in the chamber shall cause a red light to turn on at the control box. This signal shall not stop motor but shall act as a warning only, indicating service is required.

<u>PUMP IMPELLER</u> - The pump impeller shall be of the recessed Myers type to provide an open unobstructed passage through the volute for the ground solids. Impeller shall be of 85-5-5-5 bronze and shall be threaded onto stainless steel shaft. Enclosed or semi-open pump impellers which might become obstructed during grinding or

add excessive radial loads shall not be considered as equal.

GRINDER CONSTRUCTION - Grinder assembly shall consist of a single rotating grinder impeller and a single stationary shredding ring mounted directly below pump volute inlet. Grinder impeller shall thread onto shaft and shall be locked with a screw and washer. Shredding ring shall be held in place by a steel retaining clamp. Both shredding ring and grinder impeller shall be removable without dismantling pump. No adjustment of grinder assembly shall be necessary for proper grinder operation. Multiple grinder impeller assemblies requiring initial or periodic axial adjustment for proper operation shall not be considered equal. Grinder impeller and shredding ring shall be made of 440C stainless steel hardened to 58-60 Rockwell.

<u>CORROSION PROTECTION</u> - All iron castings shall be pre-treated with phosphate and chromic rinse and to be painted before machining and all machined surfaces exposed to the sewage water to be re-painted. All fasteners to be 302 stainless steel.

BEARING END CAP - Upper motor bearing cap shall be a separate casting for easy mounting and replacement.

<u>POWER CABLES</u> - Power cord and control cord shall be double sealed. The power and control conductor shall be single strand sealed with epoxy potting compound and then clamped in place with rubber seal bushing to seal outer jacket against leakage and to provide for strain pull. Cords shall withstand a pull of 300 pounds to meet U.L. requirements.

Insulation of power and control cords shall be type SOOW. Both control and power cords shall have a green carrier ground conductor that attaches to motor frame.

